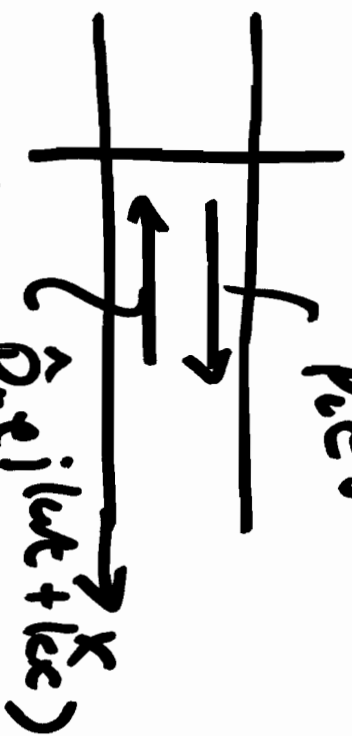


Back to Propagation in Pipes

Adopt problem-solving strategy used for complicated systems...



$$\hat{p}_c e^{j(\omega t - kx)}$$

Invoke the

narrow pipe assumption

$$\lambda \gg \sqrt{\frac{S}{\pi}}$$

\hat{p} in cross-sectional area:

$$\hat{p}(x,t) = \hat{p}_c e^{j(\omega t - kx)} + \hat{p}_r e^{j(\omega t + kx)} \quad ; p_a$$

$$\hat{u}(x,t) = \frac{\hat{p}_L}{\rho_0 c} e^{j(\omega t - kx)} - \frac{\hat{p}_R}{\rho_0 c} e^{j(\omega t + kx)} \quad ; \text{ m/s}$$

In working pipe problems, its customary to use volume velocity instead of acoustic velocity;

$$\text{Volume Velocity} = \hat{U}(x,t) = \hat{u}(x,t) S' \quad \text{m}^3/\text{s}$$

Use acoustic pressure as before, only now $\hat{U}(x,t)$ is

$$\hat{U}(x,t) = \frac{\hat{p}_L}{\rho_0 c / S'} e^{j(\omega t - kx)} + \frac{\hat{p}_R}{\rho_0 c / S'} e^{j(\omega t + kx)}$$

~~Acoustic:~~

Furthermore; we define acoustic impedance Z_0 as

$$\hat{Z}_0 = \frac{\hat{p}}{\hat{U}} = \frac{\text{acoustic pressure}}{\text{acoustic volume velocity}} = \text{acoustic impedance}$$

$\rho \hat{c} = \frac{\hat{p}}{\hat{U}} = \text{specific acoustic impedance.}$
 lower case

For a rightward travelling wave (by itself) (also called progressive wave)

$\hat{z} = \rho_0 c = z = r = \text{characteristic impedance of the medium.}$

and

$$\hat{Z}_s = \frac{\hat{P}}{\hat{U}} = \frac{\hat{P}}{\hat{U}_s} = \frac{\rho_c \hat{V}}{\rho_c \hat{V}} = \frac{\rho_c}{\rho} = \text{characteristic impedance of pipe}$$

acoustic velocity for RTPW = Z_s

In general we approach the modeling and design problem

as: $\hat{P}_i \rightarrow \hat{P}_r$

whatever Z_i

$$\frac{\hat{P}_c + \hat{P}_r}{\hat{U}_c + \hat{U}_r} = \hat{Z}_i = \frac{\hat{P}_c + \hat{P}_r}{\hat{U}_c - \hat{U}_r}$$

Multiply right-hand side by $\frac{1/\hat{p}_c}{1/\hat{p}_c}$

$$\hat{Z} = \frac{1 + \hat{r}}{Z} - \frac{\hat{r}}{Z}$$

Same fr \Rightarrow

$$\hat{r} = \frac{\hat{Z} - Z}{Z + Z}$$

$$\hat{r} = \hat{r}/\hat{p}_c$$

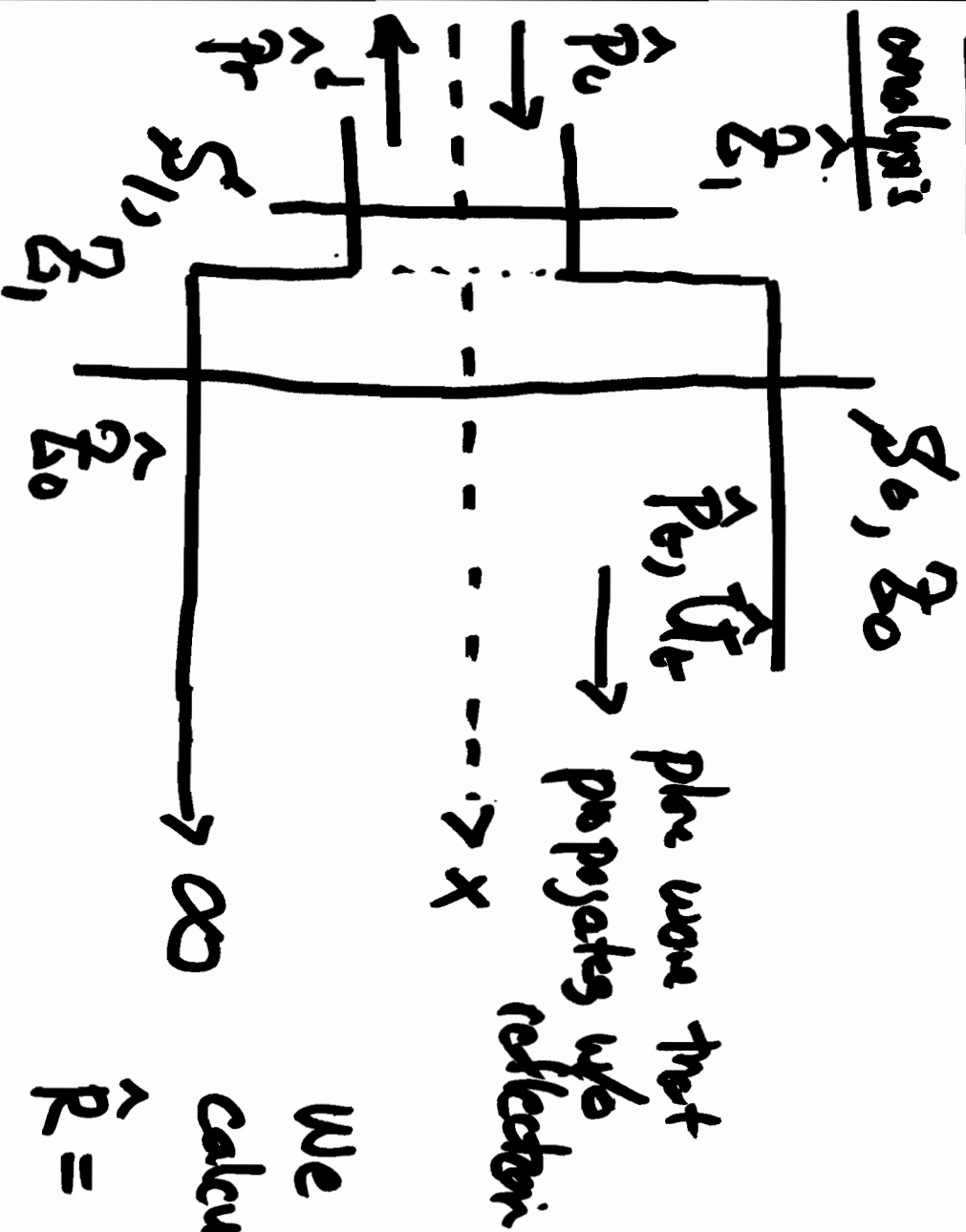
$$Z = \frac{P_c}{S}$$

$$R_I = \text{Intensity reflection} = \frac{I_r}{I_i} = |\hat{r}|^2 = \frac{I_r S}{I_i S} = \frac{\pi r}{\pi c} = R_{\pi}$$

$$T_{\pi} = \frac{I_t}{I_i} = 1 - |\hat{r}|^2$$

Design metrics

Let's consider one acoustic example and build tables for



We wish to calculate $\hat{R} = \frac{\hat{Z}_1 - Z_1}{\hat{Z}_1 + Z_1}$; $Z_1 = \frac{R_0 C}{S_1}$

We also know that $\hat{Z}_D = Z_0$ because RTPD in downstream section.

For an area change at $x=0$, we determine \hat{Z}_1 by applying the following physical boundary conditions;

continuity in $\Rightarrow \hat{p}_c + \hat{p}_r = \hat{p}_e$
acoustic pressure

divide the two

$$\frac{\hat{p}_c + \hat{p}_r}{\hat{U}_c + \hat{U}_r} = \frac{\hat{p}_e}{\hat{U}_e}$$

continuity in $\Rightarrow \hat{U}_c + \hat{U}_r = \hat{U}_e$
acoustic volume velocity

continuity in acoustic impedance across an area change $\leftarrow \hat{Z}_1 = Z_0$

change

Now we can solve the problem:

① We start with the "terminator impedance"

$$\hat{Z}_0 = \text{terminator} = Z_0 \text{ because terminator is RTPV}$$

② Invoke continuity in acoustic impedance across the area change $0 \rightarrow 1$

$$\hat{Z}_1 = \hat{Z}_0 = Z_0 \quad Z_0 = \frac{\rho_0 c}{S_0} ; Z_1 = \frac{\rho_1 c}{S_1}$$

$$\therefore R = \frac{Z_0 - Z_1}{Z_0 + Z_1} = \frac{S_1 - S_0}{S_1 + S_0}$$